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Analysis of Changes in Soot Content in Engine Oils under Operating Conditions

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Abstract: Oil has an enormous influence on the condition of the engine. Determining its degradation allows companies to maximize the availability of a specific vehicle and fleet of vehicles in general. In the evolution of engine oil degradation, one of the variables considered to be the most important is soot content. This article examines the direction and severity of soot content and dispersion changes in engine oil occurring during actual engine operation during four complete change intervals. The oil under study was operated in a city bus. It belonged to the fleet of vehicles of a transport company from new to the mileage of about 200,000 km. Soot content was determined in accordance with ASTM E2412-10, while dispersion size was determined using the dried drop test in accordance with ASTM D7899. The results obtained provide the basis for the conclusion that the direction of change in soot content in each interval is characterized by a high degree of homogeneity. With respect to the degree of soot build-up, a high level of similarity was observed between the intervals studied. The study of change in the degree of oil dispersion using the “drop on blotter” method made it possible to confirm the trend of decreasing dispersion as the run increases. The obtained results led to the development of a statistical model describing these relationships.



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Keywords: soot in oil; oil analysis; additive depletion; condition monitoring; urban buses

1. Introduction

Diesel engines are currently the main group of engines used in trucking and public transportation. The advantages of this type of engine include low fuel consumption, high durability, and reliability [1]. Despite these advantages, diesel engines have disadvantages, such as high levels of NO_x and particulate emissions. The emission of air pollutants from transport has a negative impact both on the environment and human health, as well as on climate change [2,3]. In terms of reducing air pollution, economical driving in city traffic also has great potential, and it is worth using the eco-driving style [4]. Additionally, the use of alternative fuels is one of the simpler and more effective methods of reducing exhaust emissions from diesel engines. According to studies by Ge et al., the addition of biodiesel and ethanol to diesel as a ternary blended fuel, or binary blends, can simultaneously reduce NO_x and smoke emissions, as well as particle diameter [5,6]. Another frequently used method of reducing NO_x emissions is the use of exhaust gas recirculation (EGR). However, this technology causes problems due to the increase in particulate matter entering the lubricating oil.

Only 29% of the soot produced when fuel is burned in the cylinders enters the atmosphere through the exhaust system. The remainder is deposited on the cylinder walls and piston bottoms and eventually ends up in the engine oil [7]. Soot contamination of the lubricating oil translates into increased engine wear [8]. The amount of accumulated soot in the oil is influenced by how the engine is operated, including its low or high load, ambient temperature, or idling time [9,10]. Increased soot content in engine oil can reduce lubrication efficiency by increasing viscosity, forming an abrasive substance that accelerates wear, and adsorb anti-wear additives [11–19]. Soot particles entering the oil can gather into larger clusters. They can more than double in size, as small soot particles increase from a size of less than 50 nm to more than 100 nm [20]. Therefore, effective dispersion of soot agglomerates is necessary to help mitigate the harmful effects of wear (caused by soot) on mating surfaces. Dispersant additives in lubricants reduce particle (especially soot) agglomeration through spherical stabilization, and can prevent particles and contaminants from adhering to surfaces [21]. Liu et al. [22] studied soot aggregation and the interaction between dispersant and soot using molecular dynamics simulations. The results showed that the presence of dispersant had a significant effect on disrupting soot aggregation.

Dispersion is a property that allows oil to suspend and carry away “contaminants” formed from a variety of sources, such as soot from fuel combustion, metallic particles from engine component wear, corrosion of mechanical parts, insoluble products from oil aging, etc. Dispersant particles play an important role in modifying soot particles (carbon particles from degradation) to resist their aggregation, which leads to oil thickening, mainly in heavy engines [23,24]. The accumulation of contaminants such as soot causes an increase in the viscosity of the engine oil and the formation of sludge, which can consequently lead to blockage of the oil main as well as excessive component wear [25].

The above information shows that the control of the soot content and its dispersion in engine oils is extremely important both from the point of view of oil degradation rate and replacement interval, as well as engine durability and reliability. There are many ways to measure soot in engine oils. The main technique is thermogravimetric analysis (TGA), but it has several limitations, such as a long measurement procedure and limitations in measuring small soot contents in oil [26]. Another alternative measurement technique is Fourier transform infrared spectroscopy (FTIR), which also, like TGA, has limitations in measuring small soot contents in oil [27]. In an article [28], the authors presented an alternative measurement technique that is applicable to measuring small soot contents in oil in service, based on visible ultraviolet–visible (UV–VIS) spectroscopy. Abdulqadir [29] observed that a lot of work has been devoted to analyzing soot in laboratory tests and its wear effects on engine components, while there is little work showing what effect soot has on engine oil and its additives degradation during actual road tests. These conditions, compared to laboratory tests, are characterized by less repeatability and control, while they show the problem in a more complex and thus more representative way. In addition, they can change not only depending on the conditions of their use [10], but also due to the wear of various engine components. Therefore, it is important to conduct long-term studies that enable the analysis of problems occurring not only during one oil cycle, but also covering changes in several successive cycles. In the literature, there is a very small number of papers describing research on the degradation of lubricating oil in a long-term test [30].

Therefore, the purpose of this study was to investigate the direction and intensity of changes in soot content and its dispersibility in engine oils during four consecutive engine oil change intervals. It was important to involve a vehicle belonging to the urban transport fleet in the research and to obtain oil, of which the degree of degradation is the result of the actual operating conditions of the vehicle. The obtained results led to the development of a statistical model that describes the relationship between the soot content in engine oil and the number of kilometers driven, taking into account the real conditions of vehicle operation.

2. Materials and Methods

2.1. Materials

The engine oil used in the study was operated in an Iveco city bus, model Urbanway 12M, equipped with a 228 kW Cursor 9 engine with HI-SCR technology (exhaust emission control system with passive particulate filter) meeting the Euro VI emission standard without the use of an exhaust gas recirculation (EGR) system. The test vehicle was intended for operation in public transportation in typical urban conditions. The volume of the oil sump was 34 L.

The test material included 17 engine oil samples, including one fresh oil sample. The samples were aggregated over a period of 3 years. The oil used in the engine was Petronas Urania FE LS brand oil with a viscosity grade of SAE 5W30, meeting European quality standards ACEA E4/E6/E7. In order to obtain representative oil samples, a correct and systematic sampling procedure was ensured. At the beginning of the test, a sample of new oil was tested, and then oil samples were taken periodically at successive oil change intervals. Three of the intervals ended at about 51,000 km, and one at about 44,500 km. It should be noted that the values are below the manufacturer's recommended limit of 60,000 km. The detailed data from each engine oil mileage is presented in Table 1.

Table 1. The number of kilometers traveled.

| Oil Drain Intervals | Total Vehicle Mileage (km) | Oil Mileage (km) |
|---------------------|----------------------------|---------------------|
| Interval I | 20,289 | 20,289 |
| | 29,872 | 29,872 |
| | 39,459 | 39,459 |
| | 50,780 | 50,780 (oil change) |
| Interval II | 65,345 | 14,565 |
| | 74,992 | 24,212 |
| | 85,097 | 34,317 |
| | 95,195 | 44,415 (oil change) |
| Interval III | 114,691 | 20,110 |
| | 125,179 | 30,598 |
| | 135,380 | 40,799 |
| | 146,496 | 51,915 (oil change) |
| Interval IV | 167,800 | 21,849 |
| | 175,061 | 29,179 |
| | 185,546 | 39,595 |
| | 197,961 | 52,079 (oil change) |

2.2. Test Apparatus

Soot content was measured in accordance with ASTM E2412-10 using an ERASPEC OIL mid-infrared FTIR spectrometer (Eralytics GmbH, Wien, Austria). Fourier-transform infrared spectroscopy (FTIR) is an ASTM-accepted technique for monitoring soot levels in diesel engine oils. The method works by first placing a clean oil sample in an IR cell and measuring it on the spectrometer to establish a baseline, then measured is the used oil sample [31]. Because the method measures the amount of IR light scattered rather than absorbed, the difference in baseline between the sample and the clean oil at 2000 cm^{-1} is used to determine the soot value. The FTIR method is best suited for trend analysis in the field when monitoring soot.

An automatic dispersion tester for in-service motor oils DT 100DL (AD Systems product, Saint-André-sur-Orne, France) was used to test the dispersion capacity of the oil under test. The apparatus analyzed the image of the oil droplet using a digital camera in accordance with ASTM D7899 (ASTM D7899-19, 2019). The software then scanned and analyzed all regions of the oil droplet and converted the scan into oil quality parameters. Dispersion magnitude (MD) is a key piece of information in determining the nature and content of detergents in the oil that facilitate dispersion. MD is expressed by an index of

100 (perfect dispersion) to 0 (no dispersion). Characterization of the dispersion of an oil stain was performed by determining the distance reached by the droplets from the center, or how large the central area of the drenching is and its homogeneity relative to the theoretical size of 32 mm, which is shown as a blue circle in Figure 1.

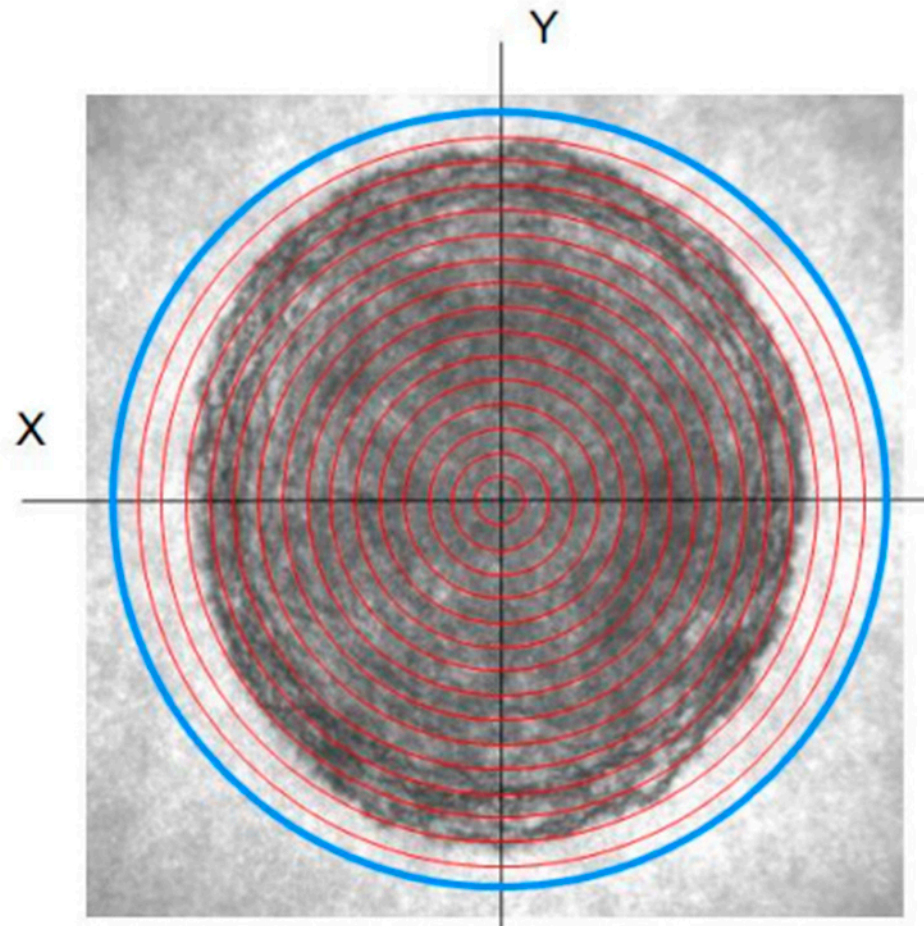


Figure 1. MD (dispersion) calculation on DT 100DL apparatus source: (<https://www.zematra.com/product/dispersancy-tester-model-dt100dl>, accessed on 11 January 2023).

2.3. Statistical Analysis

Statistica ver. 13 software (TIBCO Software Inc., Palo Alto, CA, USA, 2017) was used to analyze the results. Linear correlation coefficients were calculated between soot percentage and mileage for successive intervals. The statistical significance of the correlation coefficients was tested. Regression lines were determined and the significance of the coefficients of the lines was tested using the SimReg method. Pairwise comparisons of the runs of the lines for the intervals considered were made.

3. Results and Discussion

3.1. Changes in Soot Content in Oils

Due to continuous vehicle operation, sampling periods vary slightly. Engine oil top-ups, which were performed as part of periodic vehicle maintenance, were not recorded.

According to ASTM E2412, FTIR detects changes in the concentration of soot in engine oil in the region of about 2000 cm^{-1} . The presence of soot in engine oil causes the FTIR spectrum to shift depending on the level of soot. Figure 2 shows the recorded spectra juxtaposed with the change intervals for each cycle.

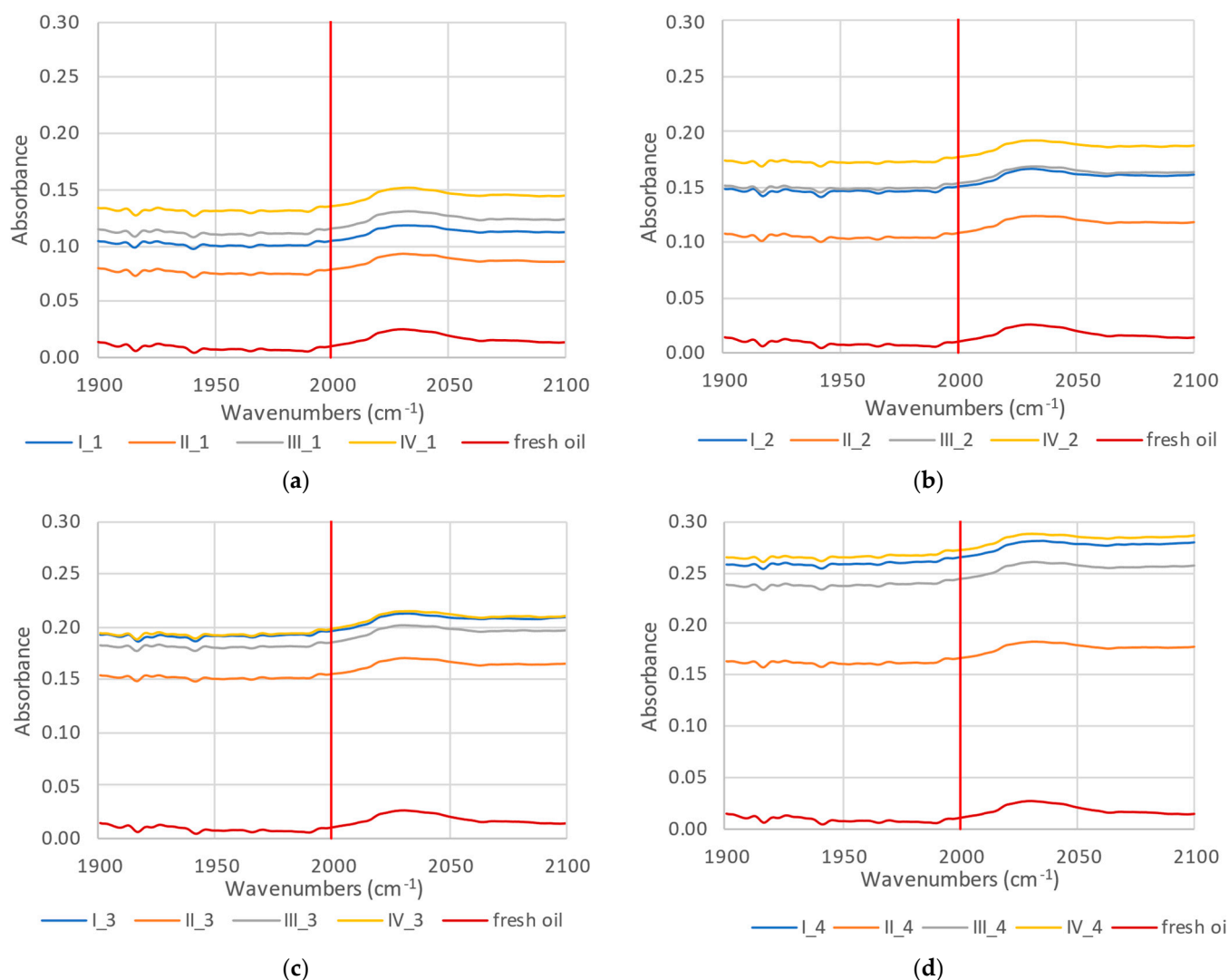


Figure 2. Spectra recorded for individual cycles at the intervals studied and for fresh oil: (a) Cycle 1, (b) Cycle 2, (c) Cycle 3, and (d) Cycle 4.

The characteristic feature of soot is the lack of any specific infrared absorption bands. Rather, the soot particles cause a general scattering of infrared radiation, which is more severe at higher wavenumbers. The darkening effect is related to the production of polymeric or polycondensation substances at higher temperatures and with the presence of impurities (especially carbon/soot). As expected, the FTIR spectra shifted with increasing levels of soot in the oils associated with the vehicle's oil service mileage. Similar observations were presented in References [24,32] examining the frequency of changing engine oil in public transport vehicles. The largest shifts in the spectrum relative to fresh oil are seen for the fourth interval for all oil intake cycles (Figure 2, yellow curve), while the smallest shifts are seen for the second interval (Figure 2, orange curve).

It is noteworthy that the shifts of the spectrum for the third and fourth oil intake cycles are similar in Intervals I and IV (Figure 2c,d).

The shifts recorded in Cycles 1 and 3 for Interval I were similar to Interval IV, while those for Cycle 2 were similar to the spectrum recorded for Interval III.

The instrument software allows the recorded spectra to be converted to soot content expressed in %.

The data presented in Table 2 show the increase in soot content at four successive engine oil change intervals in the test vehicle. The averages of the three measurements for the test sample taken in a given cycle were used for the analysis, and standard deviations

are also shown in the table. It was found that all the differences in the measurements at each interval for both the soot parameter and the dispersion size had high statistical significance.

Table 2. Results of soot content and dispersion rate in the oil samples tested.

| | Samples | Overall Vehicle Mileage (km) | | Soot (%) | Merit of Dispersancy (0–100) |
|--------------|-----------|------------------------------|---------|------------------|------------------------------|
| | | | | $\bar{x} \pm SD$ | $\bar{x} \pm SD$ |
| Interval I | 1st cycle | 20,289 | 20,289 | 0.21 ± 0.00 | 98.00 ± 2.00 |
| | 2nd cycle | 29,872 | 29,872 | 0.30 ± 0.00 | 92.67 ± 1.52 |
| | 3rd cycle | 39,459 | 39,459 | 0.40 ± 0.01 | 82.00 ± 7.21 |
| | 4th cycle | 50,780 | 50,780 | 0.51 ± 0.00 | 82.33 ± 0.58 |
| Interval II | 1st cycle | 13,951 | 65,345 | 0.16 ± 0.00 | 97.67 ± 0.58 |
| | 2nd cycle | 23,598 | 74,992 | 0.22 ± 0.00 | 93.00 ± 1.00 |
| | 3rd cycle | 33,703 | 85,097 | 0.30 ± 0.01 | 99.67 ± 0.58 |
| | 4th cycle | 43,801 | 95,195 | 0.34 ± 0.00 | 97.00 ± 1.00 |
| Interval III | 1st cycle | 19,496 | 114,691 | 0.23 ± 0.00 | 96.00 ± 4.00 |
| | 2nd cycle | 29,984 | 125,179 | 0.31 ± 0.00 | 96.00 ± 3.00 |
| | 3rd cycle | 40,185 | 135,380 | 0.37 ± 0.01 | 97.00 ± 2.00 |
| | 4th cycle | 51,301 | 146,496 | 0.49 ± 0.00 | 84.67 ± 3.21 |
| Interval IV | 1st cycle | 21,235 | 167,800 | 0.27 ± 0.00 | 99.00 ± 1.00 |
| | 2nd cycle | 28,565 | 175,061 | 0.36 ± 0.00 | 97.67 ± 0.58 |
| | 3rd cycle | 38,981 | 185,546 | 0.40 ± 0.00 | 97.00 ± 1.00 |
| | 4th cycle | 51,465 | 197,961 | 0.55 ± 0.00 | 84.33 ± 2.08 |

\bar{x} —arithmetic average, SD—standard deviation.

In all intervals, an increase in soot compactness was observed as the vehicle was driven. The highest soot content was obtained for Interval IV (Cycle 4) and was 0.55%. Slightly lower values were obtained for Interval I (Cycle 4) at 0.51% and Interval III at 0.49 (Cycle 4). This indicates that as the mileage of the vehicle, and therefore the wear of the engine, increases, the soot content of the oil also increases. This can be linked to the gradual wear of the injection apparatus. It can also be noted that the rate of accumulation of soot in the oil is similar from period to period. Differences for Cycle 4 can be seen only in the case of Interval II; however, this is due to the fact that the oil change took place at 43,801 km, so earlier than in the other periods, but the value is similar to the value at the corresponding mileage for the other intervals.

Similar results were obtained by [33] for a tractor-trailer after 40,000 km of mileage, where the value of soot in the engine oil was 0.62% (*m/m*). Comparing the obtained results with the works of other authors, in Reference [34] the authors, using a thermogravimetric analyzer (TGA), determined the soot content of small turbocharged engines, where at 5000 km mileage the soot content was at the level of 1% (*m/m*), and after 8000 km at the level of 1.5% (*m/m*), considering the obtained results to be surprisingly high, considering that the oil change interval given by the manufacturer is 15,000 km. For example, in Reference [35], the oils obtained during oil changes did not exceed 1% (*m/m*).

Statistical Analysis and Modeling Changes in Soot Content in Oils

Table 3 presents descriptive characteristics per oil sampling cycle for all oil change intervals. The cut-off value for the significance level was set at 0.05, and $p < 0.01$ was considered highly significant.

Analyzing Table 3, it was found that all the differences for variables in successive measurement periods between the first and second, second and third, and third and fourth cycles (based on data for all intervals) of oil changes for the parameter determining soot content were highly statistically significant. These results indicate an upward trend for the average values of this parameter.

Table 3. The mean values, standard deviations, and *p*-values for soot.

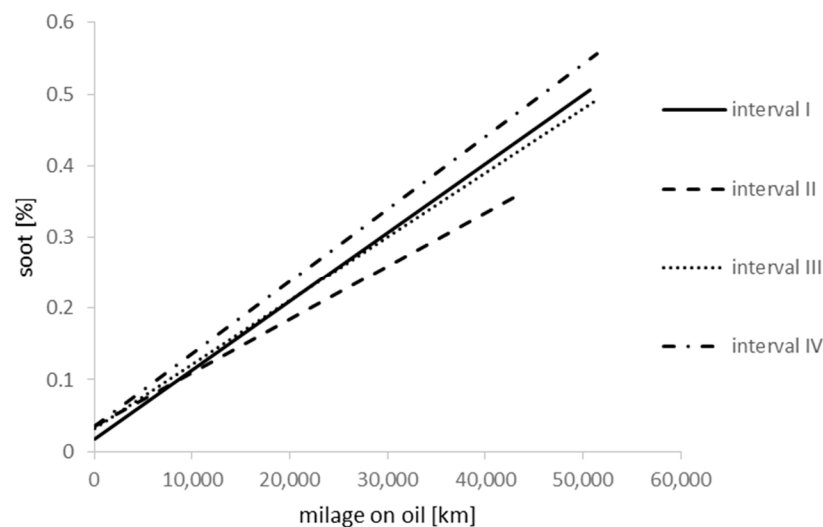
| Parameter | Average from All Four Intervals | | | | | | | | |
|-----------|---------------------------------|------------|----------|------------------|------------|----------|------------------|------------|----------|
| | 1st Cycle | 2nd Cycle | <i>p</i> | 2nd Cycle | 3rd Cycle | <i>p</i> | 3rd Cycle | 4th Cycle | <i>p</i> |
| | N = 12 | N = 12 | | N = 12 | N = 12 | | N = 12 | N = 12 | |
| | $\bar{X} \pm SD$ | | | $\bar{X} \pm SD$ | | | $\bar{X} \pm SD$ | | |
| Soot (%) | 0.22 ± 0.04 | 0.3 ± 0.05 | <0.001 | 0.3 ± 0.05 | 0.4 ± 0.04 | <0.001 | 0.4 ± 0.04 | 0.5 ± 0.08 | <0.001 |

N—number of samples tested, \bar{X} —arithmetic average, SD—standard deviation, *p*—*p*-value resulting from the application of Student's test for independent samples.

The changes in the amount of soot by mileage for each interval are described by regression lines (Table 4, Figure 3). The determined coefficients of the straights at the intervals studied are statistically significant ($p < 0.01$). Very strong statistically significant linear correlations were found between soot percentage and mileage at each of the four oil change intervals considered (Table 4). Each correlation coefficient is statistically significant ($p < 0.001$).

Table 4. Equations of estimated lines and correlation coefficients for soot quantity.

| Oil Drain Intervals | Equations | Correlation Coefficient |
|---------------------|-------------------------------------|-------------------------|
| Interval I | $S = 9.6 \times 10^{-6} M + 0.0173$ | 0.9997 |
| Interval II | $S = 7.4 \times 10^{-6} M + 0.0358$ | 0.9896 |
| Interval III | $S = 9.0 \times 10^{-6} M + 0.0314$ | 0.9959 |
| Interval IV | $S = 1.0 \times 10^{-5} M + 0.0354$ | 0.9920 |

**Figure 3.** Estimated regression lines for successive intervals.

It was checked whether the course of the straights corresponding to each interval differed significantly. The SimReg procedure [36] was used to compare the straights in pairs. Significant differences were obtained for all compared pairs of straights at a significance level less than 0.001 except for straights corresponding to Intervals I and Interval III, for which no significant difference was found (test statistic value = 1.9153 and $p = 0.9935$). Minor differences may be due to the time of year and the nature of operation between these intervals, but as shown, the direction of soot content accumulation is similar in each interval regardless of vehicle mileage, so it may be easier to control this type of pollution.

The mileage-dependent changes in soot content for the four intervals were described by linear regression equations. A common regression equation expressing soot content changes for the four oil change intervals can be created by attaching zero-one variables

to the regression model [37]. After taking into account the test result that there are no significant differences in the course of soot changes for the first and third intervals, the common regression equation has the form:

$$S = 0.0244765 + 0.0000093 M + 0.0113123 Z_1 + 0.0108823 Z_2 - 0.0000018 Z_1M + 0.0000008 Z_2M, \quad (1)$$

where the variables Z_1 and Z_2 are zero-one variables: Z_1 takes a value of 1 when the observation is from Interval II and a value of 0 for observations from other intervals, and Z_2 takes a value of 1 when the observation is from Interval IV and a value of 0 for observations from other intervals.

The very high value of the coefficient of determination of 0.989 for the above model indicates a very good fit of the estimated function to the data.

3.2. Changes in the Level of Oil Dispersion

As a dispersed solid phase, soot is kept in dispersion form by dispersant-type additives introduced into engine oils, hence causing its agglomeration to be difficult. Dispersants make up a significant part of the engine oil additive package, hence the effect of soot interaction with the dispersant is of particular importance.

Figure 4 presents sample images from the oil droplet camera of recent cycles of individual oil intervals. The camera analyzed the dispersion characteristics of the oil droplets from all measurements, and based on these images, a measure of the dispersive capacity of the oil during operation at each measurement period is presented for all four oil intervals.

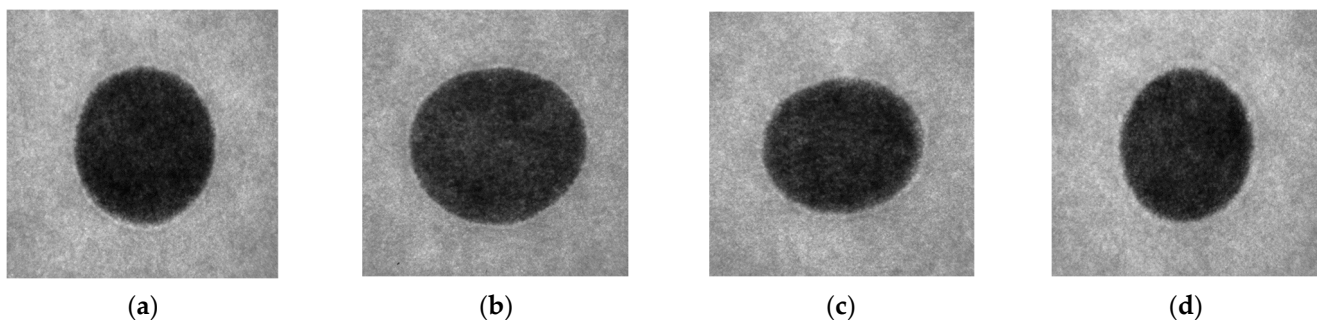


Figure 4. Changes in merit of dispersancy of engine oil tested and pictures of the last dried drops from the oil change at each interval: (a) Interval I, oil mileage = 50,780 km; (b) Interval II, oil mileage = 44,415 km; (c) Interval III, oil mileage = 51,915 km; (d) Interval IV, oil mileage = 52,079 km.

Analyzing the level of oil dispersion during the intervals studied (Table 2), we can conclude that the oil retained a high degree of dispersing capabilities for almost the entire period of operation (values close to 100). In Intervals III and IV, the levels of dispersion for the last four oil intake cycles were at the same level and amounted to 84, and a slightly lower level of 82 was observed in Interval I. Different from the other intervals, the character of the changes in dispersion magnitude was observed during the second oil change interval, where during the third intake cycle at 30,000 km, a significant increase in the value of this indicator to the level of 99.8 was observed, which may be indicative of the application of an increased dose of new oil to the oil during operation. The oil in this case, too, was changed 6000 km earlier than at the other intervals, which also affected the final result of this parameter at 97.

A similar change curve for a passenger car was observed in Reference [38].

Statistical Analysis and Modeling Changes in the Level of Oil Dispersion

Table 5 presents descriptive characteristics per oil sampling cycle for all oil change intervals. As in the case of soot content, all variables in successive measurement periods

between oil change cycles were highly statistically significant and indicate an upward trend for the average values of this parameter.

Table 5. The mean values, standard deviations, and p -values for merit of dispersancy.

| Parameter | Average from All Four Intervals | | | | | | | | |
|-----------------------------|---------------------------------|------------|--------|------------------|------------|--------|------------------|------------|--------|
| | 1st Cycle | 2nd Cycle | p | 2nd Cycle | 3rd Cycle | p | 3rd Cycle | 4th Cycle | p |
| | N = 12 | N = 12 | | N = 12 | N = 12 | | N = 12 | N = 12 | |
| | $\bar{x} \pm SD$ | | | $\bar{x} \pm SD$ | | | $\bar{x} \pm SD$ | | |
| Merit of Disperancy (0–100) | 97.7 ± 2.3 | 94.8 ± 2.7 | <0.001 | 94.8 ± 2.6 | 93.9 ± 7.9 | <0.001 | 93.9 ± 7.9 | 87.1 ± 6.3 | <0.001 |

N—number of samples tested, \bar{x} —arithmetic average, SD—standard deviation, p — p -value resulting from the application of Student's test for independent samples.

The changes in the magnitude of dispersion depending on the waveform for the first, third, and fourth intervals are described by regression lines (Table 6, Figure 5). The determined coefficients of the straights in the studied cycles are statistically significant ($p < 0.01$). Statistically significant linear correlations were found between dispersion magnitude and mileage for the first, third, and fourth oil change intervals ($p < 0.004$). For the second interval, the linear correlation coefficient (-0.1928) is not statistically significant.

Table 6. Equations of estimated lines and correlation coefficients for merit of dispersancy.

| Oil Drain Intervals | Equations | Correlation Coefficient |
|---------------------|---|-------------------------|
| Interval I | $MD = -3.7 \times 10^{-4} M + 101.0855$ | -0.8510 |
| Interval III | $MD = -2.1 \times 10^{-4} M + 100.3022$ | -0.6963 |
| Interval IV | $MD = -2.4 \times 10^{-4} M + 101.7997$ | -0.7363 |

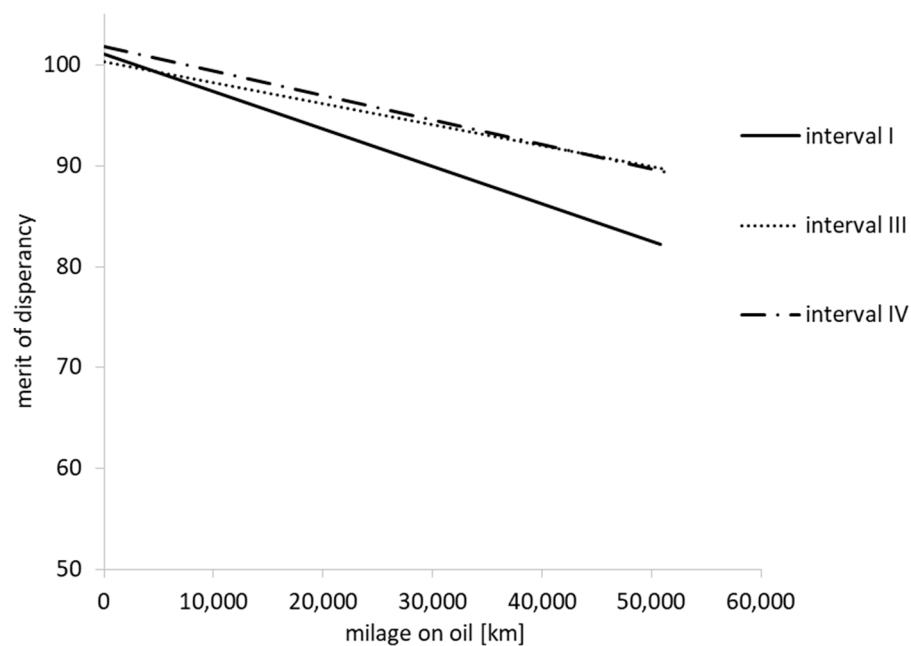


Figure 5. Estimated regression lines for successive intervals.

It was checked whether the course of the straights corresponding to each interval differed significantly [36]. Significant differences were obtained for the compared pairs of straights corresponding to Intervals I and III and Intervals I and IV at a significance level of

less than 0.004, while no significant difference was found for straights corresponding to Intervals III and IV (test statistic value = 0.6196 and $p = 0.8265$).

For Intervals I, III, and IV, the changes in the amount of dispersion depending on the waveform were described by linear regression equations. In addition, the result of the test indicated that there were no significant differences in the course of changes in dispersion magnitude for the IIIrd and IVth intervals. The common regression equation for the first, third, and fourth oil change intervals is of the form

$$MD = 101.04698 - 0.0002246 M + 0.0385072Z_1 - 0.0001466 Z_1M, \quad (2)$$

where the variable Z_1 takes the value of 1 for observations coming from Interval I and the value of 0 for observations from Intervals III and IV.

The coefficient of determination for the determined model common to the three intervals is 0.618.

4. Conclusions

The field test carried out on a selected bus from the vehicle fleet provides a deeper understanding of how the soot content of engine oil changes during operation. The observation concerned four consecutive oil change intervals (mileage of about 200,000 km) over a 3-year period, during which engine oil samples were taken periodically. The presented work fills the diagnosed gap in the literature on the subject, as it has been observed that there are few works presenting the degradation processes of engine oils during actual operating conditions.

The results obtained provide a basis for the conclusion that the direction of changes in soot content is the same in each interval, and these changes are similar to each other. Soot accumulation does not significantly differ between the intervals studied. Statistical analysis made it possible to confirm the significance of changes in the soot content of the oil in relation to the vehicle's operating mileage.

The data obtained indicate that it is possible to develop a statistical model of changes in the soot content of oil, which could be used to predict the behavior of engine oil during operation, which was realized in the presented work.

Investigations of the change in the degree of oil dispersion using the "drop on blotter" method made it possible to confirm the trend of decreasing dispersion as the mileage increases. Statistical analysis confirmed the significance of changes in the level of dispersion in relation to the vehicle's operating mileage. However, the results are not as conclusive as in the case of changes in soot compactness. No significant differences were found in the course of changes in dispersion volume for only two intervals. Thus, the model obtained in this study had a low correlation coefficient of 0.618 and was based on only three intervals, which should be considered an area for improvement based on more data in future studies.

The authors are in the course of further research based on the presented methodology. These tests include checking other engines, oil categories, and number of change intervals. This will make it possible to check the validity of the obtained models.

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